



Stability of Converter-Based Power Systems

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Outline

- Power Electronics in Power Systems
- Characteristics of Machines vs. Converters
- Converter-Based Power System Stability
- Small-Signal Sequence Impedance Theory and Applications
- Summary and Future Development

Power Electronics in Power Systems





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Power Electronics in Power Systems



- Power Electronics is the Key to These New Developments
- 100% Renewable \rightarrow >100% Converter-Based Power System

Converter-Based Power System





Machines (& Transformers) vs. Converters

• Slow or No Control

• Fast Control is Essential



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Machines (& Transformers) vs. Converters

• Overloading Comes Free

• Overloading at High Cost





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Power System Stability



Frequency (Hz)

Converter-Based Power System Stability



Frequency (Hz)

EMT Stability

- Study of System Stability in the EMT Frequency Range Requires EMT Models
 - Fundamental-Frequency Models cannot Describe Fast Control & Dynamics
- EMT Simulation is a Useful Tool but Simulation is not Enough
- Analytical and Small-Signal Methods are Required for General Stability Study and System Design → Small-Signal EMT Models
- Direct Linearization of EMT Models Leads to Linear Time Periodic Models That cannot be Handled by Practical Control Methods

 $[x(t) + \Delta x][y(t) + \Delta y] = x(t)y(t) + x(t) \cdot \Delta y + y(t) \cdot \Delta x$

Harmonic Linearization

- Linearization Along a Periodic Operation Trajectory (Harmonic)
- Frequency-Domain Models Small-Signal Sequence Impedances

Perturbation Method	Domain	Perturbation
Amplitude (& Phase) Modulation	Time	$[V_r + \Delta v_r(t)] \cos \omega_1 t - [V_i + \Delta v_i(t)] \sin \omega_1 t$
	Frequency	$[V_r + \Delta V_r \cos(\omega_p t + \varphi_r)] \cos \omega_1 t - [V_i + \Delta V_i \cos(\omega_p t + \varphi_i)] \sin \omega_1 t$
Superimposed Harmonic	Time	$V_1 \cos(\omega_1 t + \varphi_1) + \Delta v(t)$
	Frequency	$V_1 \cos(\omega_1 t + \varphi_1) + \Delta V_p \cos(\omega_p t + \varphi_p)$





Impedance-Based System Stability Theory



$$I_g(s) = \frac{I_c(s)/Z_g(s)}{\frac{1}{Z_c(s)} + \frac{1}{Z_g(s)}} - \frac{V_g(s)}{Z_c(s) + Z_g(s)} = \left[\frac{I_c(s) - \frac{V_g(s)}{Z_c(s)}}{\frac{1}{Z_c(s)}} \right] \cdot \frac{1}{1 + \frac{Z_g(s)}{Z_c(s)}}$$

- System Modeling Based on Impedance
- Converter-Grid Forms a Feedback Loop by Virtue of Impedance
- Stability Requires the Resulting Effective Loop Gain to Satisfy Nyquist Criterion
- System is Stable if both **Positive and Negative Sequence** Subsystems are Stable

Type-III Turbine with HVDC Converter



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Offshore HVDC Converter & Cable Network



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HVDC Converter Resonance with Grid



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Research Summary

- Development of Analytical Impedance Models
 - PV Inverters; Type III & Type IV Turbines
 - Classical HVDC, MMC-Based HVDC & FACTS
- Impedance-Based System Stability Studies
 - PV Inverters and Wind Turbines Connected to Weak Grids
 - Offshore Wind Farms with HVDC Transmission
 - HVDC Converters for Bulk Power Transmission
 - Multi-Terminal HVDC
- Damping of Resonance and System Stabilization

Converter-Based Power System Testbed



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Applications and Practical Development

- Root Cause Analysis & Solutions to System Resonances
 - German (TenneT) North Sea Wind Farms with HVDC 2014-2015
 - Hami (China State Grid) Renewable Development Zone 2015-2016
 - Facebook Data Center Power Systems 2017-2018



Applications and Practical Development

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- New Grid Codes for Renewable Energy and HVDC Development
- Impedance-Based Specifications; Measurement and Verification



Summary and Future Development

- Converters are Very Different from Machines
- Converter-Based Power Systems Face New Stability Challenges
 - Require New Modeling and System Analysis Methods
- Frequency-Domain Methods Based on Small-Signal Sequence Impedances
- Large-Signal and Transient Stability; Fault and Protection

Characteristics	Small-Signal Stability	Large-Signal Stability
Fast Control		
Overload Capacity		



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